

U.S. DEPARTMENT OF COMMERCE PATENT AND TRADEMARK

ATTORNEY'S DOCKET NUMBER

TRANSMITTAL LETTER TO THE UNITED STATES

DESIGNATED/ELECTED OFFICE (DO/EO/US)

32860-000265/US U.S. APPLICATION NO. (If known, see 37 CFR 1.5

CONCERNING A FILING UNDER 35 U.S.C. 371

10/0%

INTERNATIONAL FILING DATE PCT/DE00/02071 June 26, 2000 July 9, 1999 TITLE OF INVENTION ELECTRICAL BONDING PROTECTED AGAINST OXIDATION ON THE GAS COMBUSTION SIDE OF A HIGH-TEMPERATURE FUEL CELL. APPLICANT(S) FOR DO/FO/US Thomas IANSING Applicant herewith submits to the United States Designated/Elected Office (DO/EO/US) the following items and other information: This is a FIRST submission of items concerning a filing under 35 U.S.C. 371. This is a SECOND or SUBSEQUENT submission of items concerning a filing under 35 U.S.C. 371. This express request to begin national examination procedures (35 U.S.C. 371(f)) at any time rather than delay examination until the expiration of the applicable time limit set in 35 U.S.C. 371(b) and PCT Articles 22 and 39 (1). The US has been elected by the expiration of 19 months from the priority date (Article 31). A copy of the International Application as filed (35 U.S.C. 371(c)(2)) a. Is transmitted herewith (required only if not transmitted by the International Bureau). WO 00/ b. has been transmitted by the International Bureau. is not required, as the application was filed in the United States Receiving Office (RO/US). An English language translation of the International Application as filed (35 U.S.C. 371(c)(2)). a. is transmitted herewith. has been previously submitted under 35 U.S.C. 154(d)(4) 7 Amendments to the claims of the International Application under PCT Article 19 (35 U.S.C. 371(c)(3)). are transmitted herewith (required only if not transmitted by the International Bureau). have been transmitted by the International Bureau. have not been made; however, the time limit for making such amendments has NOT expired. d. A have not been made and will not be made. An English language translation of the amendments to the claims under PCT Article 19 (35 U.S.C. 371(c)(3)). An oath or declaration of the inventor(s) (35 U.S.C. 371(c)(4)). An English language translation of the annexes of the International Preliminary Examination Report under PCT Article 36 (35 U.S.C. 371(c)(5)). Items 11. to 20. below concern document(s) or information included: 11. An Information Disclosure Statement under 37 CFR 1.97 and 1.98-1449 and International Search Report (PCT/ISA/210) in German An assignment document for recording. A separate cover sheet in compliance with 37 CFR 3.28 and 3.31 is included. A FIRST preliminary amendment. A SECOND or SUBSEQUENT preliminary amendment. A substitute specification. 16 A change of power of attorney and/or address letter. 17. A computer-readable form of the sequence listing in accordance with PCT Rule 13ter.2 and 35 U.S.C. 1.821-1.825. A second copy of the published international application under 35 U.S.C. 154(d)(4).

A second copy of the English language translation of the international application under 35 U.S.C. 154(d)(4).

19.

Other items or information:

1) One (1) sheets of Formal Drawings

U.S. APPLICATION NO (if linews, see 37 C	77447	INTERNAT	IONAL APPLICATION NO			ATTORNEY'S DOCKET NUMBER			
TOKE	T 0 de 0 3 1125 DITENTATIONAL APPLICATION NO PCT/DE00/02071		71		32860-000265/US				
21. The following fees					CAL	CULATIONS	PTO USE ONLY		
BASIC NATIONAL FEE (37 CFR 1.492(a)(1)-(5):									
Neither international preliminary examination fee (37 CFR 1.482)									
nor international search fee (37 CFR 1.445(a)(2)) paid to USPTO									
and International Search Report not prepared by the EPO or JPO									
International prelimina	International preliminary examination fee (37 CFR 1.482) not paid to								
USPTO but Internation	nal Search Report pr	epared b	y the EPO or JPO	\$890.00					
			1.482) not paid to USPTO						
but international search	1 ree (37 CFR 1.445	(a)(2)) pa	aid to USPTO	\$710.00	l				
International prelimina	rv examination fee	37 CFR	1 482) paid to HSPTO						
			icle 33(1)-(4)	\$690.00	l				
	**			**********	1				
International prelimina									
			3(1)-(4)	\$100.00	s	890.00			
ENTER API	PROPRIATE I	BASIC	FEE AMOUNT =		Ľ				
Surcharge of \$130.00 f				☒ 30	s	130.00			
months from the earlies					Ľ_	150.00			
La CLAIMS	NUMBER FIL	ED	NUMBER EXTRA	RATE					
Total Claims	20 - 20 =		0	X \$18.00	\$	0			
Independent Claims	2 - 3 =		0	X \$80.00	\$	0			
MÜLTIPLE DEPENDI	ENT CLAIM(S) (if	applicabl	e) None	+ \$270.00	\$	0			
F (1)	TOTAL OF ABOVE CALCULATIONS = \$ 1,020.00								
Applicant claims small entity status. See 37 CFR 1.27. The fees indicated above are reduced by 1/2.									
179			SUB	TOTAL =	\$	1,020.00			
Processing fee of \$130.	00 for furnishing the	English		20 []30					
months from the earliest claimed priority date (37 CFR 1.492(f)).									
1.4			TOTAL NATIONA	L FEE =	,\$	1,020.00			
Fee for recording the enclosed assignment (37 CFR 1.21(h)). The assignment must be accompanied by an appropriate cover sheet (37 CFR 3.28, 3.31). \$40.00 per property +									
		(e) Civi	TOTAL FEES ENC		\$	1,020.00			
						mount to be:			
						refunded	\$		
						charged	\$		
a. A check in the amount of \$ to cover the above fees is enclosed.									
b. Please charge my Deposit Account. No. 08-0750 in the amount of \$1,020.00 to cover the above fees. A triplicate copy of this sheet is enclosed.									
c. The Commissioner is hereby authorized to charge any additional fees which may be required, or credit any overpayment to Deposit Account No. 08-0750.									
NOTE: Where an appropriate time limit under 37 CFR 1.494 or 1.495 has not been met, a petition to revive (37 CFR									
1.137(a) or (b)) must be filed and granted to restore the application to pending status.									
Send all correspondence to:									
Harness, Dickey & Pierce, P.L.C - Customer No. 30596 Post Office Box 8910									
Reston, Virginia 201				,	\cap	1.0			
				//	/ /	11 /1	110		
Date: January 9, 2002 By						45_ 1			
Donald J. Daley, #34,313							1		
кла						V			

PATENT 32860-000265/US

IN THE U.S. PATENT AND TRADEMARK OFFICE

Applicants:

Thomas JANSING

Int'l Application:

PCT/DE00/02071

Application No.:

NEW

Filed: For: January 9, 2002

ELECTRICAL BONDING PROTECTED AGAINST OXIDATION

ON THE GAS COMBUSTION SIDE OF A HIGH-TEMPERATURE

FUEL CELL

PRELIMINARY AMENDMENT

Assistant Commissioner for Patents Washington, DC 20231

January 9, 2002

Sir:

The following preliminary amendments and remarks are respectfully submitted in connection with the above-identified amplication.

IN THE ABSTRACT

Please replace the Abstract with the attached revised Abstract.

IN THE CLAIMS

Please replace the original claims with the following new claims:

1. A fuel cell, comprising:

a cathode:

an electrolyte;

an anode;

interconnector plates; and

at least one metallic mesh, inserted between the anode and an interconnector plate for flexibly making contact, wherein the at least one metallic mesh is protected against oxidation.

- The fuel cell as claimed in claim 1, wherein the at least one metallic mesh is coated with an oxidation-resistant protective layer.
 - The fuel cell as claimed in claim 1, wherein the mesh is a coated nickel mesh.
- The fuel cell as claimed in claim 1, wherein the mesh is a coated stainless steel
 mesh.
- The fuel cell as claimed in claim 2, wherein the protective layer includes chromium.
- The fuel cell as claimed in claim 2, wherein the protective layer includes chromium carbide.
- The fuel cell as claimed in claim 6, wherein at least one of Cr₃C₂, CrC, Cr₇C₃ and Cr₂₃C₆ is used as chromium carbide.

Please add the following new claims:

- -- 9. The fuel cell as claimed in claim 2, wherein the mesh is a coated nickel mesh.
- The fuel cell as claimed in claim 2, wherein the mesh is a coated stainless steel mesh.
- The fuel cell as claimed in claim 3, wherein the protective layer includes chromium.

- The fuel cell as claimed in claim 4, wherein the protective layer includes chromium.
- The fuel cell as claimed in claim 3, wherein the protective layer includes chromium carbide.
- 14. The fuel cell as claimed in claim 4, wherein the protective layer includes chromium carbide.
- The fuel cell as claimed in claim 5, wherein the protective layer includes chromium carbide.
 - 16. A fuel cell stack, comprising:

a plurality of fuel cells, each fuel cell including,

a cathode.

an electrolyte,

an anode,

interconnector plates, and

at least one metallic mesh, inserted between the anode and an interconnector plate for flexibly making contact, wherein the at least one metallic mesh is protected against oxidation.

- The fuel cell stack of claim 16, wherein the at least one metallic mesh is coated with an oxidation-resistant protective layer.
 - 18. The fuel cell stack of claim 16, wherein the mesh is a coated nickel mesh.
 - 19. The fuel cell stack of claim 17, wherein the mesh is a coated nickel mesh.
- The fuel cell stack of claim 16, wherein the mesh is a coated stainless steel mesh.

REMARKS

Claims 1-20 are now present in this application, with new claims 9-20 being added by the present Preliminary Amendment. It should be noted that the amendments to original claims 1-8 of the present application are non-narrowing amendments, made solely to place the claims in proper form for U.S. practice and not to overcome any prior art or for any other statutory considerations. For example, amendments have been made to broaden the claims; remove reference numerals in the claims; remove the European phrase "characterized in that"; remove multiple dependencies in the claims; and to place claims in a more recognizable U.S. form, including the use of the transitional phrase "comprising" as well as the phrase "wherein". Other such non-narrowing amendments include rearranging apparatus-type claims (setting elements forth in separate paragraphs) into a more recognizable U.S. form. Again, all amendments are non-narrowing and have been made solely to place the claims in proper form for U.S. practice and not to overcome any prior art or for any other statutory considerations.

SUBSTITUTE SPECIFICATION

In accordance with 37 C.F.R. §1.125, a substitute specification has been included in lieu of substitute paragraphs in connection with the present Preliminary Amendment. The substitute specification is submitted in clean form, attached hereto, and is accompanied by a marked-up version showing the changes made to the original specification. The changes have been made in an effort to place the specification in better form for U.S. practice. No new matter has been added by these changes to the specification. Further, the substitute specification includes paragraph numbers to facilitate amendment practice as requested by the U.S. Patent and Trademark Office.

Docket No.: 32860-000265/US

CONCLUSION

Accordingly, in view of the above amendments and remarks, an early indication of the allowability of each of claims 1-20 in connection with the present application is earnestly solicited.

Should there be any outstanding matters that need to be resolved in the present application, the Examiner is respectfully requested to contact Donald J. Daley at the telephone number of the undersigned below.

If necessary, the Commissioner is hereby authorized in this, concurrent, and future replies, to charge payment or credit any overpayment to Deposit Account No. 08-0750 for any additional fees required under 37 C.F.R. § 1.16 or under 37 C.F.R. § 1.17; particularly, extension of time fees.

Respectfully submitted,

HARNESS, DICKEY & PIERCE, P.L.C

Donald J. Daley, Ree

P.O. Box 8910

Reston, Virginia 20195

(703) 390-3030

DJD:kna

ABSTRACT OF THE DISCLOSURE

A fuel cell or a fuel cell stack includes cathodes arranged in parallel in layers, an electrolyte, anodes and interconnector plates. Further, at least one metallic mesh is included, which is inserted between an anode and an interconnector plate for flexibly making contact. The at least one metallic mesh is protected against oxidation.

New PCT Application Docket No. 32860-000265/US

SUBSTITUTE SPECIFICATION

ELECTRICAL BONDING PROTECTED AGAINST OXIDATION ON THE GAS COMBUSTION SIDE OF A HIGH-TEMPERATURE FUEL CELL

[0001] This application is the national phase under 35 U.S.C. § 371 of PCT International Application No. PCT/DE00/02071 which has an International filing date of June 26, 2000, which designated the United States of America, the entire contents of which are hereby incorporated by reference.

Field of the Invention

[0002] The invention generally relates to a fuel cell or a fuel cell stack.

Background of the Invention

[0003] It is known that connecting a plurality of fuel cells in series results in a fuel cell stack. Such a fuel cell stack includes an interconnector plate, a protective layer, a contact layer, a cathode, an electrolyte, an anode, a further contact layer and a further interconnector plate. The interconnector plate forms a unit with the protective and contact layers, which are each sprayed on. Cathode, electrolyte and anode form the electrolyte/electrodes unit. The corresponding units are laid in parallel, in layers, on top of one another and the same sequence is repeated a number of times.

[0004] Cathode, electrolyte and anode form an electrolyte/electrodes unit. In each case one electrolyte/electrodes unit, lying between adjacent interconnector plates, together with the contact and protective layers which bear directly against the electrolyte/electrodes unit on both sides, forms a high-temperature fuel cell. The fuel cell also includes those sides of each of the two interconnector plates which bear against the protective layer or the contact layers. The interconnector plates usually consist of CrFe5 with 1% of Y oxide, known as an ODS alloy.

[0005] Gas ducts, through which, firstly, the fuel gas, for example hydrogen or methane (natural gas), and, secondly, oxygen or air is passed, are formed in the interconnector plate. The hydrogen is passed to the anode side, the oxygen or air to the cathode side. These gases are passed through at a relatively low excess pressure of less than 1 bar.

[0006] The planar design of the high-temperature fuel cell requires the contact between the electrodes in both gas spaces to be over as much of the surface as possible. On the cathode side, contact with the electrode is ensured by a contact layer made from La perovskite, e.g. La₈SrO_{0.2}MnO₃. This perovskite is stable in air. By contrast, on the fuel cell side contact with the electrode, i.e. the anode, is more difficult to achieve. However, complete contact with the

anode is necessary, on account of the low transverse conductivity of the anode. The anode is produced by the screen-printing process and is therefore not planar over the entire surface,
 which means that a flexible contact-making element which has very good electrical conductivity and must be able to withstand an operating period of approximately 40,000 h is
 required.

[0007] The prior art provides for nickel meshes to be used as flexible contact-making elements. By way of example, a fine nickel mesh and a coarse nickel mesh are laid on top of one another and are spot-welded to one another, so that a flexible interlayer with good contact is created.

[0008] A drawback which has emerged in the prior art is that an oxide layer, which in the area without material-to-material bonding consists of Cr_2O_3 (Cr_xO_y), and in the area with material-to-material bonding probably consists of an CrNi spinel, grows in the region of direct contact between the nickel mesh and CrFe5 both during soldering of the fuel cell stack and during operation of the fuel cell or of the fuel cell stack. These oxide layers are thought to be largely responsible for the excessively high series resistances of the high-temperature fuel cells. Consequently, the electrical output is greatly adversely affected.

[0009] Moreover, during soldering of the fuel cell stack using a glass solder in an air atmosphere, the nickel mesh is oxidized at the surface of the wires, to a depth of a few μ m into the interior of the wires. The formation of nickel(II) oxide (NiO), which has a volume which is approximately 16% greater than nickel, leads to an increase in thickness of the overall mesh assembly of around 10-40 μ m (depending on the soldering conditions). The increase in thickness in the oxidized region of the wire is more than 16%, since the NiO formed is porous. During the oxidation, the nickel meshes and their wires sinter together. During the subsequent reduction of the nickel mesh, the original thickness of the mesh assembly is restored or even, under certain circumstances, reduced further.

[0010] During this reduction, the nickel wires sinter together, so that a reduction in the desired flexibility and also a reduction in the thickness occur, which is undesirable. The reduction in thickness may also lead to contact separation, which can lead to damage to components.

SUMMARY OF THE INVENTION

[0011] The invention is based on an object of further developing a fuel cell or a fuel cell stack in such a manner that the reduction in thickness and flexibility of the nickel mesh(es) is avoided. As such, contact between the anode and the interconnector plate which is as complete as possible can be achieved.

[0012] This object is achieved by patent claim 1. Advantageous refinements of the fuel cell will emerge from subclaims 2-8.

[0013] In one embodiment, at least one metallic mesh, which is protected against oxidation, is inserted between anode and interconnector plate in order to flexibly make contact.

•• [0014] Meshes of this type as the contact layer have the advantage that they can no longer be oxidized, and consequently the increase in thickness is also eliminated. Since no oxidation •• has taken place, there is also no need for a reduction of the metallic meshes. Further, the associated drawbacks, such as for example contact separations during the reduction in thickness or flexibility losses, do not occur. On account of the fact that the oxidation/reduction process does not take place, the original thickness and flexibility of the oxidation-protected meshes is retained, so that a contact layer which makes very good contact between anode and interconnector is created. Moreover, a reduction in the thickness of the metallic meshes as the service life progresses is prevented.

[0015] The metallic meshes are expediently coated with an oxidation-resistant protective layer. In this way, the metallic meshes, e.g. nickel meshes, remain unaffected both in terms of their composition and in terms of their mechanical and electrical properties, i.e., inter alia, they remain substantially flexible, do not bring about any change in thickness and substantially retain their advantageous properties. It is advantageous in this case that, before being introduced as flexible contact layer, the metallic meshes are subjected to the coating process. The assembly with the other components and the soldering are then to be carried out in the customary way.

[0016] Coated nickel meshes can be provided as metallic meshes. The nickel meshes satisfy the requirements with regard to flexibility and also electrical conductivity.

[0017] The metallic meshes provided may also be coated stainless steel meshes, which have the property of only being superficially oxidized, down to a depth of approximately 5 μ m. The stainless steel meshes are in this case likewise coated with an oxidation-resistant protective layer. A further advantage of the stainless steel meshes is that their coefficient of thermal expansion is well matched to the thermal characteristics of the components of the fuel cell stack. This property is highly advantageous in particular when the fuel cell operates at high temperatures.

[0018] The protective layer advantageously contains chromium, and is therefore matched to the chemical composition of the interconnector plate.

[0019] The protective layer advantageously includes chromium carbide, which is highly electrically conductive and adheres very well to the metallic mesh. Moreover, a chromium carbide layer is very resistant to corrosion at corresponding oxygen partial pressures on the fuel gas side. Furthermore, these layers are stable when methane or gases derived from carbon, which are later charge media on the fuel gas side of the high-temperature fuel cell, are used.

[0020] A further advantage of the coating with chromium carbide consists in the fact that, when using gases which are derived from carbon and are passed through the gas ducts on the anode side of the interconnector plates, minor constituents of the protective layers are restored again by the gases derived from carbon. Therefore, the chromium carbide layer is particularly favorable in thermodynamic terms.

[0021] By way of example, the chromium carbide used may be Cr_3C_2 , CrC, Cr_7C_3 or $Cr_{23}C_6$. [0022] It is also possible for the protective layer of the metallic meshes to include chromium nitride

[0023] The protective layer expediently has a thickness d of $0.1-10 \mu m$, so that, firstly, sufficient resistance to oxidation is provided and, secondly, the flexibility of the metallic meshes is scarcely restricted.

BRIEF DESCRIPTION OF THE DRAWINGS

[0024] The invention is explained in more detail with reference to an advantageous exemplary embodiment shown in the drawings, in which:

- Fig. 1 shows a diagrammatic cross-sectional illustration of the layers of a fuel cell, and
- Fig. 2 shows an enlarged, diagrammatic cross-sectional illustration of a coated nickel mesh.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

[0025] A fuel cell 1, in one embodiment corresponding to the diagrammatic illustration in Fig. 1, includes an interconnector plate 5', a protective layer 8, a contact layer 9, a cathode 2, an electrolyte 3, an anode 4, two metallic meshes 6, 6' which rest on top of one another, and an interconnector plate 5. Such a fuel cell 1 as shown in Fig. 1 can be part of a fuel cell stack. The components are preferably arranged in parallel, in layers, on top of one another. The metallic meshes can be nickel, and the metallic mesh 6 is preferably thinner than the mesh 6'.

[0026] The nickel meshes 6, 6' are protected against oxidation, in order to avoid oxidation of these meshes, which usually occurs during soldering of the entire fuel cell stack. The oxidation of the nickel meshes is linked to an increase in thickness, the original thickness of the mesh assembly being restored during the subsequent reduction operation. This may lead to contact separations, which can cause damage to components. Moreover, after the reduction the nickel wires become sintered together, so that the desired flexibility is reduced. Accordingly, the oxidation-protected meshes avoid the oxidation/reduction process of the mesh assembly and the associated drawbacks. The original flexibility and the thickness of the meshes can be retained, so that complete contact between anode 4 and the contact layer of the

nickel meshes 6, 6' and the interconnector plate 5 is created. Moreover, a reduction in thickness of the nickel meshes 6, 6' during operation of the fuel cell 1 is prevented.

• [0027] As can be seen from Fig. 1 and Fig. 2, the nickel meshes 6, 6' are provided with an oxidation-resistant protective layer 7. This coating may be carried out before assembly of the individual components. Therefore, the original, advantageous properties of the nickel meshes 6, 6' are not changed by an oxidation process and a subsequent reduction process. Fig. 2 shows an enlarged excerpt illustrating the coating of a nickel mesh 6 or 6'.

[0028] Stainless steel meshes, which have the advantage of a coefficient of longitudinal thermal expansion being matched to the components of the high-temperature fuel cell, may also be provided instead of the nickel meshes 6, 6°.

[0029] The protective layer 7 includes chromium carbide, which has the advantage that, when using gases derived from carbon, which are introduced through the gas ducts on the anode side of the interconnector plates 5, 5', constituents which disappear from the protective layers are restored again by the gases derived from carbon.

[0030] Cr₃C₂, CrC, Cr₇C₃ or Cr₂₃C₆ or similar chromium carbides with different valencies can be used as chromium carbides.

[0031] The protective layer 7 has a thickness d of 0.1-10 μ m, in order to reliably prevent oxidation and to scarcely affect the flexibility of the nickel meshes 6, 6'.

[0032] The invention being thus described, it will be obvious that the same may be varied in many ways. Such variations are not to be regarded as a departure from the spirit and scope of the invention, and all such modifications as would be obvious to one skilled in the art are intended to be included within the scope of the following claims.

_Description

Against Oxidation

Stechnical Booking Against Oxidation
Oxidation Protected (electrical contact making element on the fuel (gas) Side of a High-Temperature Euel Cell

(ZO71 5 Filed 6/24/00)

> C U

> į.

ļ.£ NJ

U

O

ļ.

Uī

stack. having the further features of the preamble of -patent claim 1.

BACKGROUND OF THE INJENTION

It is known that connecting a plurality of fuel cells 10 in series results in a fuel cell stack. which, in order, includes comprises an interconnector plate, a protective layer, a contact layer, a cathode, an electrolyte, an anode, a further contact layer and a further interconnector plate. The interconnector plate forms a unit with the 15 protective and contact layers, which are each sprayed Cathode, electrolyte and anode electrolyte/electrodes unit. The corresponding units are laid in parallel, in layers, on top of one another 20 and the same sequence is repeated a number of times.

Cathode. electrolyte and anode form an electrolyte/electrodes unit. In each case one electrolyte/electrodes unit, lying between adjacent interconnector plates, together with the contact and protective layers which bear directly against the electrolyte/electrodes unit on both sides, forms a high-temperature fuel celly, which, also includes those electrolyte/electrodes unit sides of each of the two interconnector plates which 30 bear against the protective layer or the contact layers. The interconnector plates usually consist of CrFe5 with 1% of Y oxide, known as an ODS alloy.

Gas ducts, through which, firstly, the fuel gas, for example hydrogen or 35 methane (natural secondly, oxygen or air is passed, are formed in the interconnector plate. The hydrogen is passed to the anode side, the oxygen or air to the cathode side.

10

15

20

25

30

35

These gases are passed through at a relatively low excess pressure of less than 1 bar.

The planar design of the high-temperature fuel cell requires the contact between the electrodes in both gas spaces to be over as much of the surface as possible. On the cathode side, contact with the electrode is ensured by a contact layer made from La perovskite, e.g. $La_8SrO_{0.2}MnO_3$. This perovskite is stable in air. By contrast, on the fuel cell side contact with the electrode, i.e. the anode, is more difficult achieve. However, complete contact with the anode is necessary, on account of the low conductivity of the anode. The anode is produced by the screen-printing process and is therefore not planar over the entire surface, which means that a flexible contact-making element which has very good electrical conductivity and must be able to withstand an operating period of approximately 40,000 h is required.

The prior art provides for nickel meshes to be used as flexible contact-making elements. By way of example, a fine nickel mesh and a coarse nickel mesh are laid on top of one another and are spot-welded to one another, so that a flexible interlayer with good contact is created.

A drawback which has emerged in the prior art is that an oxide layer, which in the area without material-tomaterial bonding consists of Cr_2O_3 $(\text{Cr}_x\text{O}_y)\,,$ and in the with material-to-material bonding consists of an CrNi spinel, grows in the region of direct contact between the nickel mesh and CrFe5 both during soldering of the fuel cell stack and during operation of the fuel cell or of the fuel cell stack. oxide layers are thought to be responsible for the excessively high series resistances of the high-temperature fuel cells. Consequently, the electrical output is greatly adversely affected.

15

20

Moreover, during soldering of the fuel cell stack using a glass solder in an air atmosphere, the nickel mesh is oxidized at the surface of the wires, to a depth of a few μm into the interior of the wires. The formation of nickel(II) oxide (NiO), which has a volume which is approximately 16% greater than nickel, leads to an increase in thickness of the overall mesh assembly of around 10-40 μm (depending on the soldering conditions). The increase in thickness in the oxidized region of the wire is more than 16%, since the NiO formed is porous. During the oxidation, the nickel meshes and their wires sinter together. During the subsequent reduction of the nickel mesh, the original thickness of the mesh assembly is restored or even, under certain circumstances, reduced further.

During this reduction. t.he nickel wires sinter together. SO that a reduction in the desired flexibility and also a reduction in the thickness occur, which is undesirable. The reduction in thickness may also lead to contact separation, which can lead to damage to components.

SUMMARY OF THE INVENTION

The invention is based on the object of further developing a fuel cell or a fuel cell stack having the features of the preamble of patent claim 1 in such a manner that the reduction in thickness and flexibility of the nickel mesh(es) is avoided, so that contact between the anode and the interconnector plate which is as complete as possible can be achieved.

This object is achieved by the characterizing features -of patent claim 1. Advantageous refinements of the fuel 35 cell will emerge from subclaims 2-8.

The essence of the invention is regarded as being that a new metallic mesh, which is protected against

oxidation, is inserted between anode and interconnector plate in order to flexibly make contact.

Meshes of this type as the contact layer have the advantage that they can no longer be oxidized, consequently the increase in thickness eliminated. Since no oxidation has taken place, there is also no need for a reduction of the metallic meshes g. further, with the associated drawbacks, such as for example contact separations during the reduction in thickness or flexibility losses, do not occur. On account of the fact that the oxidation/reduction process does not take place, the original thickness and flexibility of the oxidation-protected meshes is retained, so that a contact layer which makes very good contact between anode and interconnector is created. Moreover, reduction in the thickness of the metallic meshes as the service life progresses is prevented.

The metallic meshes are expediently coated with an 20 oxidation-resistant protective layer. In this way, the metallic meshes, e.g. nickel meshes, remain unaffected both in terms of their composition and in terms of their mechanical and electrical properties, i.e., inter 25 alia, they remain substantially flexible, do not bring about any change in thickness and substantially retain their advantageous properties. It is advantageous in this case that, before being introduced as flexible contact layer, the metallic meshes are subjected to the coating process. The assembly with the other components and the soldering are then to be carried out in the customary way.

Coated nickel meshes can be provided as metallic meshes. The nickel meshes satisfy the requirements with 35 regard to flexibility and also electrical conductivity.

The metallic meshes provided may also be stainless steel meshes, which have the property of only being superficially oxidized, down to a depth of approximately 5 $\mu m.$ The stainless steel meshes are in this case likewise coated with an oxidation-resistant protective layer. A further advantage of the stainless steel meshes is that their coefficient of thermal expansion is well matched to the thermal characteristics of the components of the fuel cell stack. This property is highly advantageous in particular when the fuel cell operates at high temperatures.

The protective layer advantageously contains chromium, and is therefore matched to the chemical composition of the interconnector plate.

15

10

5

The protective layer advantageously consists of chromium carbide, which is highly electrically conductive and adheres very well to the metallic mesh. Moreover, a chromium carbide layer is very resistant to corrosion at corresponding oxygen partial pressures on the fuel gas side. Furthermore, these layers are stable when methane or gases derived from carbon, which are later charge media on the fuel gas side of the high-temperature fuel cell, are used.

25

30

A further advantage of the coating with chromium carbide consists in the fact that, when using gases which are derived from carbon and are passed through the gas ducts on the anode side of the interconnector plates, minor constituents of the protective layers are restored again by the gases derived from carbon. Therefore, the chromium carbide layer is particularly favorable in thermodynamic terms.

35 By way of example, the chromium carbide used may be Cr_3C_2 , CrC, Cr_7C_3 or $Cr_{23}C_6$.

It is also possible for the protective layer of the metallic meshes to $\frac{\text{consist}}{\text{of}}$ chromium nitride.

The protective layer expediently has a thickness d of 0.1-10 μm , so that, firstly, sufficient resistance to oxidation is provided and, secondly, the flexibility of the metallic meshes is scarcely restricted.

BRIST DESCRIPTION OF THE DRAWINGS

The invention is explained in more detail reference to an advantageous exemplary embodiment shown in the drawings, in which:

10

15

20

25

30

35

Fig. 1 shows diagrammatic cross-sectional illustration of the layers of a fuel cell, and

Fig. 2 shows an enlarged, diagrammatic cross-sectional illustration of a coated nickel mesh.

, in one embodinet DETAILED DESCRIPTION OF THE PREFENCED EMBODIMENTS The fuel cell stack of the fuel cell 1 corresponding to the diagrammatic illustration in Fig. 1, comprises interconnector plate 5', a protective laver contact layer 9, a cathode 2, an electrolyte anode 4, two nickel meshes 6, 6' which rest on top of another, and an interconnector plate anged in parallel, metallic meshes can be a top of one another. The nickely mesh 6 is thinner than the nickel mesh 6'.

nickel meshes 6, 6' are protected oxidation, in order to avoid oxidation of these meshes, which usually occurs during soldering of the entire fuel cell stack. The oxidation of the nickel meshes is linked to an increase in thickness, the original thickness of the mesh assembly being restored during the subsequent reduction operation. This may lead to contact separations, which can cause damage components. Moreover, after the reduction the nickel wires become sintered together, so that the desired flexibility is reduced. Accordingly, the oxidationprotected meshes avoid the oxidation/reduction process of the mesh assembly and the associated drawbacks. The

15

20

25

original flexibility and the thickness of the meshes can be retained, so that complete contact between anode 4 and the contact layer of the nickel meshes 6, 6' and the interconnector plate 5 is created. Moreover, a reduction in thickness of the nickel meshes 6, 6' during operation of the fuel cell 1 is prevented.

As can be seen from Fig. 1 and Fig. 2, the nickel meshes 6, 6' are provided with an oxidation-resistant protective layer 7. This coating may be carried out before assembly of the individual components. Therefore, the original, advantageous properties of the nickel meshes 6, 6' are not changed by an oxidation process and a subsequent reduction process. Fig. 2 shows an enlarged excerpt illustrating the coating of a nickel mesh 6 or 6'.

Stainless steel meshes, which have the advantage of a coefficient of longitudinal thermal expansion being matched to the components of the high-temperature fuel cell, may also be provided instead of the nickel meshes 6, 6'.

includes

The protective layer 7 consists of chromium carbide, which has the advantage that, when using gases derived from carbon, which are introduced through the gas ducts on the anode side of the interconnector plates 5, 5', constituents which disappear from the protective layers are restored again by the gases derived from carbon.

30

 Cr_3C_2 , CrC, Cr_7C_3 or Cr_{23}C_6 or similar chromium carbides with different valencies can be used as chromium carbides.

35 The protective layer 7 has a thickness d of 0.1-10 µm, in order to reliably prevent oxidation and to scarcely affect the flexibility of the nickel meshes 6, 6'.

15

25

35

What is claimed is:

(athodes (2) arranged in parallel in layers outside (3) arranged in parallel in layers outside (4) and interconnector plates (5, 5'), as well as at least one metallic mesh (6, 6') which is inserted between anode (4) and interconnector plate (5) for flexibly making contact, characterized in that the at least one metallic mesh (6, 6') is protected against oxidation.

The fuel cell as claimed in claim 1, characterized in that the at least one metallic mesh (6, 6') is coated with an oxidation-resistant protective layer (7).

The fuel cell as claimed in one of claims 1 for 2, (characterized in that the mesh (6, 6) is a coated nickel mesh.

4. The fuel cell as claimed in one of the preceding claims, Characterized in that the mesh (6, 6') is a coated stainless steel mesh.

The fuel cell as claimed in claims 2-4.

Characterized in that the protective layer (7)

contains (Enromium.

6. The fuel cell as claimed in one of the preceding claims 2-J, Characterized in that the protective layer (7) consists of chromium carbide.

in that Crsc2, CrC, Cr₇C₃ Otl Cr₂₃C₆ is used as chromium carbide.

The fuel cell as claimed in one of the preceding claims, characterized in that the protective layer

(7) has a thickness (d) of approximately 0.1-10 μm .

New

9. Same as 3, but dep on 2

10. Same as 4, but dep on 2

Il some or 5, but dep on 3

12. " 5

13. 1 6 " 3

14, 6 1

15. " 6 " 5

16. A fuel cell stack, comprising including, ga flurality of fiel cells, each fire cell including, (some body as claim)

17. The fuel cell stack of claim 16, (Samborate cl. 27)

18. The finel 'cell stack of claim 16,

19. sac as 18, but dep on 17

20. The fuel cell stack of claim 16, [some booky as cl. 4] Abstract

Oxidation-protected electrical contact-making element on the fuel gas side of a high-temperature fuel coll

The invention relates to a fuel cell (1) or a fuel cell stack having cathodes (2) arranged in parallel in layers, lelectrolyte (3), anodes (4) and interconnector plates (5, 54), as well as at least one metallic mesh (6, 64) which is inserted between anode (4) and interconnector plate (5) for flexibly making contact, wherein the at least one metallic mesh (6, 64) is protected against oxidation.

Fig. 1

1) prts

Description

Oxidation-protected electrical contact-making element on the fuel gas side of a high-temperature fuel cell

The invention relates to a fuel cell or a fuel cell stack having the further features of the preamble of patent claim 1.

10 It is known that connecting a plurality of fuel cells in series results in a fuel cell stack which, in order, comprises an interconnector plate, a protective layer, a contact layer, a cathode, an electrolyte, an anode, a further contact layer and a further interconnector 15 plate. The interconnector plate forms a unit with the protective and contact layers, which are each sprayed Cathode, electrolyte and anode form electrolyte/electrodes unit. The corresponding units are laid in parallel, in layers, on top of one another 20 and the same sequence is repeated a number of times.

Cathode, electrolyte and anode form an electrolyte/electrodes unit. In each case electrolyte/electrodes unit, lying between adjacent 25 interconnector plates, together with the contact and protective layers which bear directly against the electrolyte/electrodes unit on both sides, forms a high-temperature fuel cell, which also includes those sides of each of the two interconnector plates which bear against the protective layer or the contact 30 layers. The interconnector plates usually consist of CrFe5 with 1% of Y oxide, known as an ODS alloy.

Gas ducts, through which, firstly, the fuel gas, for sample hydrogen or methane (natural gas), and, secondly, oxygen or air is passed, are formed in the interconnector plate. The hydrogen is passed to the anode side, the oxygen or air to the cathode side.

20

25

30

35

These gases are passed through at a relatively low excess pressure of less than 1 bar.

The planar design of the high-temperature fuel cell requires the contact between the electrodes in both gas spaces to be over as much of the surface as possible. On the cathode side, contact with the electrode is ensured by a contact layer made from La perovskite, e.g. LagSrOq.2MnO3. This perovskite is stable in air. By 10 contrast, on the fuel cell side contact with the electrode, i.e. the anode, is more difficult achieve. However, complete contact with the anode is necessary, on account of the low transverse conductivity of the anode. The anode is produced by the screen-printing process and is therefore not planar over the entire surface, which means that a flexible contact-making element which has very good electrical conductivity and must be able to withstand an operating period of approximately 40,000 h is required.

The prior art provides for nickel meshes to be used as flexible contact-making elements. By way of example, a fine nickel mesh and a coarse nickel mesh are laid on top of one another and are spot-welded to one another, so that a flexible interlayer with good contact is created.

A drawback which has emerged in the prior art is that an oxide layer, which in the area without material-tomaterial bonding consists of Cr_2O_3 (Cr_xO_v), and in the with material-to-material bondina consists of an CrNi spinel, grows in the region of direct contact between the nickel mesh and CrFe5 both during soldering of the fuel cell stack and during operation of the fuel cell or of the fuel cell stack. oxide layers are thought to be responsible for the excessively high series resistances of the high-temperature fuel cells. Consequently, the electrical output is greatly adversely affected.

15

35

Moreover, during soldering of the fuel cell stack using a glass solder in an air atmosphere, the nickel mesh is oxidized at the surface of the wires, to a depth of a few μ m into the interior of the wires. The formation of nickel(II) oxide (NiO), which has a volume which is approximately 16% greater than nickel, leads to an increase in thickness of the overall mesh assembly of around 10-40 μm (depending on the soldering conditions). The increase in thickness in the oxidized region of the wire is more than 16%, since the NiO formed is porous. During the oxidation, the nickel meshes and their wires sinter together. During the subsequent reduction of the nickel mesh, the original thickness of the mesh assembly is restored or even, under certain circumstances, reduced further.

During this reduction, the nickel wires sinter together, so that a reduction in the desired 20 flexibility and also a reduction in the thickness occur, which is undesirable. The reduction in thickness may also lead to contact separation, which can lead to damage to components.

25 The invention is based on the object of further developing a fuel cell or a fuel cell stack having the features of the preamble of patent claim 1 in such a manner that the reduction in thickness and flexibility of the nickel mesh(es) is avoided, so that contact 30 between the anode and the interconnector plate which is

as complete as possible can be achieved.

This object is achieved by the characterizing features of patent claim 1. Advantageous refinements of the fuel cell will emerge from subclaims 2-8.

The essence of the invention is regarded as being that at least one metallic mesh, which is protected against

oxidation, is inserted between anode and interconnector plate in order to flexibly make contact.

Meshes of this type as the contact layer have the advantage that they can no longer be oxidized, consequently the increase in thickness is eliminated. Since no oxidation has taken place, there is also no need for a reduction of the metallic meshes, with the associated drawbacks, such as for example 10 contact separations during the reduction in thickness or flexibility losses, do not occur. On account of the fact that the oxidation/reduction process does not take place, the original thickness and flexibility of the oxidation-protected meshes is retained, so that contact layer which makes very good contact between anode and interconnector is created. Moreover, reduction in the thickness of the metallic meshes as the service life progresses is prevented.

The metallic meshes are expediently coated with an oxidation-resistant protective layer. In this way, the metallic meshes, e.g. nickel meshes, remain unaffected both in terms of their composition and in terms of their mechanical and electrical properties, i.e., inter alia, they remain substantially flexible, do not bring about any change in thickness and substantially retain their advantageous properties. It is advantageous in this case that, before being introduced as flexible contact layer, the metallic meshes are subjected to the coating process. The assembly with the other components and the soldering are then to be carried out in the customary way.

Coated nickel meshes can be provided as metallic meshes. The nickel meshes satisfy the requirements with regard to flexibility and also electrical conductivity.

The metallic meshes provided may also be coated stainless steel meshes, which have the property of only

being superficially oxidized, down to a depth of approximately 5 μm . The stainless steel meshes are in this case likewise coated with an oxidation-resistant protective layer. A further advantage of the stainless steel meshes is that their coefficient of thermal expansion is well matched to the thermal characteristics of the components of the fuel cell stack. This property is highly advantageous particular when the fuel cell operates at high temperatures.

The protective layer advantageously contains chromium, and is therefore matched to the chemical composition of the interconnector plate.

15

10

The protective layer advantageously consists of chromium carbide, which is highly electrically conductive and adheres very well to the metallic mesh. Moreover, a chromium carbide layer is very resistant to corrosion at corresponding oxygen partial pressures on the fuel gas side. Furthermore, these layers are stable when methane or gases derived from carbon, which are later charge media on the fuel gas side of the high-temperature fuel cell, are used.

25

30

20

A further advantage of the coating with chromium carbide consists in the fact that, when using gases which are derived from carbon and are passed through the gas ducts on the anode side of the interconnector plates, minor constituents of the protective layers are restored again by the gases derived from carbon. Therefore, the chromium carbide layer is particularly favorable in thermodynamic terms.

35 By way of example, the chromium carbide used may be Cr_3C_2 , CrC, Cr_7C_3 or Cr_23C_5 .

It is also possible for the protective layer of the metallic meshes to consist of chromium nitride.

The protective layer expediently has a thickness d of $0.1\text{--}10~\mu\text{m}$, so that, firstly, sufficient resistance to oxidation is provided and, secondly, the flexibility of the metallic meshes is scarcely restricted.

The invention is explained in more detail with reference to an advantageous exemplary embodiment shown in the drawings, in which:

10

15

20

- Fig. 1 shows a diagrammatic cross-sectional illustration of the layers of a fuel cell, and
- Fig. 2 shows an enlarged, diagrammatic cross-sectional illustration of a coated nickel mesh.

The fuel cell stack of the fuel cell 1 corresponding to the diagrammatic illustration in Fig. 1 comprises an interconnector plate 5', a protective layer 8, a contact layer 9, a cathode 2, an electrolyte 3, an anode 4, two nickel meshes 6, 6' which rest on top of one another, and an interconnector plate 5, these components being arranged in parallel, in layers, on top of one another. The nickel mesh 6 is thinner than the nickel mesh 6'.

nickel meshes 6, 6' are protected against oxidation, in order to avoid oxidation of these meshes. which usually occurs during soldering of the entire 3.0 fuel cell stack. The oxidation of the nickel meshes is linked to an increase in thickness, the original thickness of the mesh assembly being restored during the subsequent reduction operation. This may lead to contact separations, which can cause components. Moreover, after the reduction the nickel 35 wires become sintered together, so that the desired flexibility is reduced. Accordingly, the oxidationprotected meshes avoid the oxidation/reduction process of the mesh assembly and the associated drawbacks. The

30

original flexibility and the thickness of the meshes can be retained, so that complete contact between anode 4 and the contact layer of the nickel meshes 6, 6' and the interconnector plate 5 is created. Moreover, a reduction in thickness of the nickel meshes 6, 6' during operation of the fuel cell 1 is prevented.

As can be seen from Fig. 1 and Fig. 2, the nickel meshes 6, 6' are provided with an oxidation-resistant protective layer 7. This coating may be carried out before assembly of the individual components. Therefore, the original, advantageous properties of the nickel meshes 6, 6' are not changed by an oxidation process and a subsequent reduction process. Fig. 2 shows an enlarged excerpt illustrating the coating of a nickel mesh 6 or 6'.

Stainless steel meshes, which have the advantage of a coefficient of longitudinal thermal expansion being matched to the components of the high-temperature fuel cell, may also be provided instead of the nickel meshes 6, 6'.

The protective layer 7 consists of chromium carbide, which has the advantage that, when using gases derived from carbon, which are introduced through the gas ducts on the anode side of the interconnector plates 5, 5', constituents which disappear from the protective layers are restored again by the gases derived from carbon.

 $\text{Cr}_3\text{C}_2,~\text{CrC},~\text{Cr}_7\text{C}_3$ or Cr_{23}C_6 or similar chromium carbides with different valencies can be used as chromium carbides.

35 The protective layer 7 has a thickness d of 0.1-10 µm, in order to reliably prevent oxidation and to scarcely affect the flexibility of the nickel meshes 6, 6'.

Patent claims

5

10

15

20

25

- A fuel cell (1) or a fuel cell stack, having cathodes (2) arranged in parallel in layers, electrolyte (3), anodes (4) and interconnector plates (5, 5'), as well as at least one metallic mesh (6, 6') which is inserted between anode (4) and interconnector plate (5) for flexibly making contact, characterized in that the at least one metallic mesh (6, 6') is protected against oxidation.
- The fuel cell as claimed in claim 1, characterized in that the at least one metallic mesh (6, 6') is coated with an oxidation-resistant protective layer (7).
- The fuel cell as claimed in one of claims 1 or 2, characterized in that the mesh (6, 6') is a coated nickel mesh.
- 4. The fuel cell as claimed in one of the preceding claims, characterized in that the mesh (6, 6') is a coated stainless steel mesh.
- The fuel cell as claimed in claims 2-4, characterized in that the protective layer (7) contains chromium.
- 30 6. The fuel cell as claimed in one of the preceding claims 2-5, characterized in that the protective layer (7) consists of chromium carbide.
- 7. The fuel cell as claimed in claim 6, characterized in that Cr_3C_2 , CrC, Cr_7C_3 or $Cr_{23}C_6$ is used as chromium carbide.
 - The fuel cell as claimed in one of the preceding claims, characterized in that the protective layer

(7) has a thickness (d) of approximately 0.1-10 $\mu m.$

Abstract

Oxidation-protected electrical contact-making element on the fuel gas side of a high-temperature fuel cell

The invention relates to a fuel cell (1) or a fuel cell stack, having cathodes (2) arranged in parallel in layers, electrolyte (3), anodes (4) and interconnector plates (5, 5'), as well as at least one metallic mesh (6, 6') which is inserted between anode (4) and interconnector plate (5) for flexibly making contact, wherein the at least one metallic mesh (6, 6') is protected against oxidation.

Fig. 1

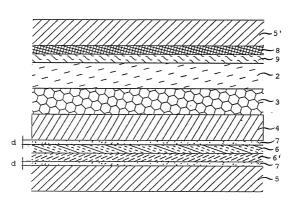


FIG. 1

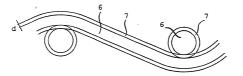


FIG. 2

Declaration and Power of Attorney For Patent Application Erklärung Für Patentanmeldungen Mit Vollmacht German Language Declaration

Als nachstehend benannter Erfinder erkläre ich hiermit an Eides Statt:

As a below named inventor, I hereby declare that:

dass mein Wohnsitz, meine Postanschrift, und meine Staatsangehörigkeit den im Nachstehenden nach meinem Namen aufgeführten Angaben entsprechen, My residence, post office address and citizenship are as stated below next to my name,

dass ich, nach bestem Wissen der ursprüngliche, erste und alleinige Erfinder (falls nachstehend nur ein Name angegeben ist) oder ein ursprünglicher, erster und Miterfinder (falls nachstehend mehrere Namen aufgeführt sind) des Gegenstandes bin, für den dieser Antrag gestellt wird und für den ein Patent beantragt wird für die Erfindune mit dem Titel: I believe I am the original, first and sole inventor (if only one name is listed below) or an original, first and joint inventor (if plural names are listed below) of the subject matter which is claimed and for which a patent is sought on the invention entitled

Oxidationsgeschützte elektrische Kontaktierung auf der Brenngasseite der Hochtemperatur-Brennstoffzelle

ELECTRICAL BONDING PROTECTED AGAINST OXIDATION ON THE GAS COMBUSTION SIDE OF A HIGH TEMPERARTURE FUEL CELL >

deren Beschreibung

the specification of which

(zutreffendes ankreuzen)

☐ hier beigefügt ist.

☐ am _28. Juni 2000als
PCT internationale Anmeldung
PCT Anmeldungsnummer PCT/DE00/02071
eingereicht wurde und am
abgeändert wurde (falls stasächlich abgeändert).

Ich bestätige hiermit, dass ich den Inhalt der obigen Patentanmeldung einschliesslich der Ansprüche durchgesehen und verstanden habe, die eventuell durch einen Zusatzantrag wie oben erwähnt abgeändert wurde. I hereby state that I have reviewed and understand the contents of the above identified specification, including the claims as amended by any amendment referred to above.

Ich erkenne meine Pflicht zur Offenbarung irgendwelcher Informationen, die für die Prüfung der vorliegenden Anmeldung in Einklang mit Absatz 37, Bundesgesetzbuch, Paragraph 1.56(a) von Wichtigkeit sind, an I acknowledge the duty to disclose information which is material to the examination of this application in accordance with Title 37, Code of Federal Regulations, \$1.56(a).

Ich beanspruche hiermit ausländische Prioritätsvorteile gemäse Abschnitt 35 der Zivliprozessordnung der Vereinigten Staaten, Paragraph 119 aller unten angegebenen Auslandsammeldungen für ein Patent oder eine Erfindersurkunde, und habe auch alle Auslandsammeldungen für ein Patent oder eine Erfindersurkunde nachstehend gekennzeichnet, die ein Anmeldedatum haben, das vor dem Anmeldedatum der Anmeldung liegt, für die Proirität beansprucht wird. I hereby claim foreign priority benefits under Title 35, United States Code, §119 of any foreign application(s) for patent or inventor's certificate listed below and have also identified below any foreign application for patent or inventor's certificate having a filing date before that of the application on which priority is claimed:

	G	erman Langua	age Declaration		*****
Prior foreign appp Priorität beanspru				Priority	Claimed
19932192.2 (Number) (Nummer)	DE (Country) (Land)	09.07.1999 (Day Month Ye (Tag Monat Jah	ar Filed)	Yes Ja	No Nein
(Number) (Nummer)	Country) (Land)	(Day Month Year Filed) (Tag Monat Jahr eingereicht)		Yes Ja	□ No Nein
(Number) (Nummer)	(Country) (Land)	(Day Month Year Filed) (Tag Monat Jahr eingereicht)		Yes Ja	□ No Nein
prozessordnung of 120, den Vorzug dungen und falls of dieser Anmeldu amerikanischen I	hiermit gemäss Absatz 3 der Vereinigten Staaten, g aller unten aufgeführ der Gegenstand aus jede ung nicht in einer Patentanmeldung laut of Absatzes 35 der Zivilprox	Paragraph ten Anmel- m Anspruch früheren dem ersten	I hereby claim the b Code. §120 of any below and, insofar a claims of this applic United States appli the first paragraph §122, I acknowled	United States a as the subject ma cation is not disc cation in the ma of Title 35, Uni	pplication(s) liste atter of each of the closed in the price anner provided be ited States Code

der Vereinigten Staaten, Paragraph 122 offenbart ist, erkenne ich gemäss Absatz 37, Bundesgesetzbuch, Paragraph 1.56(a) meine Pflicht zur Offenbarung von Informationen an, die zwischen dem Anmeldedatum der früheren Anmeldung und dem nationalen oder PCT internationalen Anmeldedatum dieser Anmeldung bekannt geworden sind.

information as defined in Title 37. Code of Federal Regulations, §1.56(a) which occured between the filing date of the prior application and the national or PCT international filing date of this application.

(Application Serial No.) (Anmeldeseriennummer) (Filing Date D, M, Y) (Anmeldedatum T, M, J) (patentiert, anhangig, (patented, pending, aufgegeben) abandoned) (Application Serial No.) (Filing Date D.M.Y) (Status) (Anmeldeseriennummer) (Anmeldedatum T, M; J) (patentiert, anhängig, (patented, pending abandoned)

Ich erkläre hiermit, dass alle von mir in der vorliegenden Erklärung gemachten Angaben nach meinem besten Wissen und Gewissen der vollen Wahrheit entsprechen, und dass ich diese eidesstattliche Erklärung in Kenntnis dessen abgebe, dass wissentlich und vorsätzlich falsche Angaben gemäss Paragraph 1001, Absatz 18 der Zivilprozessordnung der Vereinigten Staaten von Amerika mit Geldstrafe belegt und/oder Gefängnis bestraft werden koennen, und dass derartig wissentlich und vorsätzlich falsche Angaben die Gültigkeit der vorliegenden Patentanmeldung oder eines darauf erteilten Patentes gefährden können.

I hereby declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true, and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code and that such willful false statements may jeopardize the validity of the application or any patent issued thereon

Page 2

The state of the s

German Language Declaration

Customer No. 30596

VERTRETUNGSVOLLMACHT: Als benannter Erfinder beauftrage ich hiermit den nachstehend benannten Patentanwalt (oder die nachstehend benannten Patentanwälte) und/oder Patent-Agenten mit der Verfolgung der vorliegenden Patentanmeldung sowie mit der Abwicklung aller damit verbundenen Geschäfte vor dem Patent- und Warenzeichenamt: (Name und Registrationsnummer anfihren)

POWER OF ATTORNEY: As a named inventor, I hereby appoint the following attorney(s) and/or agent(s) to prosecute this application and transact all business in the Patent and Trademark Office connected therewith. (list name and registration number)

And I hereby appoint

Telefongespräche bitte richten an: (Name und Telefonnummer)	Direct Telephone Calls to: (name and telephonumber)
	Ext
Postanschrift:	Send Correspondence to:
Harness, Dickey 12355 Sunrise Valley Drive, Telephone: +1 703 390 3030 a	<u>Suite 350 20191 Reston, Va.</u> and Facsimile + <u>1 703 390 302</u> 0
Voller Name des einzigen oder ursprünglichen Erfinders:	
	Full name of sole or first inventor:
Thomas Jansing	Thomas Jansing
Unterschrift des Erfinders Datum X Z7. 12. 2001	Inventor's signature Date
Wohnsitz	Residence
Nürnberg DE ★	Nürnberg,
Staatsangehörigkeit	Citizenship
DE /	DE
Postanschrift	Post Office Addess
Kilianstrasse 46	Kilianstrasse 46
90425 Nürnberg	90425 Nürnberg
Voller Name des zweiten Miterfinders (falls zutreffend):	Full name of second joint inventor, if any:
Unterschrift des Erfinders Datum	Second Inventor's signature Date
Wohnsitz	Residence
Staatsangehorigkeit	Cilizenship
Postanschrift	Post Office Address
(Bitte entsprechende Informationen und Unterschriften im Falle von dritten und weiteren Miterfindern angeben).	(Supply similar information and signature for third and subsequent joint inventors).
Pag	e 3
	Patent and Trademark Office-U.S. Department of COMMERCE